## Study on Linear Vibration Model of Shield TBM **Cutterhead Driving System**

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In this paper, a general linear time-varying multiple-axis (LTVMA) vibration model of shield tunnel boring machine (TBM) cutterhead driving system is established. The corresponding multiple inputs and multiple outputs (MIMO) state-space model is also presented. The linear vibration model is analysed, and the vibration-torque transfer function matrix and the vibration-torque static gain matrix are obtained. The linear vibration model is simulated, and the physical parameters' effects on the vibration response are investigated. A preliminary approach is proposed to reduce vibration by increasing motor rotor inertia and viscous damped. The LTVMA vibration model provides a solid foundation for fault detection and diagnosis (FDD), as long as the health monitoring of cutterhead driving system.

 $\mathbf{F_i}$ 

gear

Elastic mesh force of the pinion-i and large

## NOMENCLATURE

		$\mathbf{r}_{i}$	radius of pinion-i
n	The number of cutterhead driving motors;	M <sub>ci</sub>	Elastic mesh torque of the pinion-i and large
$\mathbf{q}$	the reducer speed reduction ratio	0,1	gear
$\mathbf{J_{d,i}}$	i-th induction motor rotor inertia after equiva-	Di	Relative position of the pinion-i and large gear
	lent coupling-i	k;	Mesh stiffness of the pinion-i and large gear
$\mathbf{b_{d,i}}$	i-th induction motor rotor viscous damped af-	 C:	Mesh damped of the pinion-i and large gear
	ter equivalent coupling-i	m ·	Mass of the pinion-i
$\mathbf{J_{z,i}}$	Inertia of the <i>i</i> -th coupling between motor-i	ութ,լ Ն	support stiffness of ninion i
	and reducer-i	к <sub>у,i</sub>	support summed of pinion i
$\mathbf{b}_{\mathbf{z},\mathbf{i}}$	Viscous damped of the i-th coupling between	$c_{y,i}$	Mass of the large gear
т	motor-1 and reducer-1	ling Le	support stiffnass of large gear
J <sub>r,i</sub> h	i th induction motor rotor viscous domaed	$\mathbf{K}_{\mathbf{y},\mathbf{m}}$	support summed of large gear
$D_{r,i}$	I and a serie anti-	$\mathbf{c}_{\mathbf{y},\mathbf{m}}$	The contact direction (line of action direction)
J <sub>m</sub>	Large gear mertia	<b>y</b> i	vibration displacement of i-th pinion
b <sub>m</sub>	large gear viscous damped	i	The lange of the l
$\mathbf{r_m}$	large gear radius	$\mathbf{y}_{\mathbf{m}}$	The large gear's contact vibration displace-
$\theta_{\mathbf{p},\mathbf{i}}$	Angular displacement of 1-th active pinion		tion
$\theta_{\mathbf{i}}$	angular displacement of i-th motor rotor	Тт	Shield TBM cutterhead's load torque
$\theta_{\mathbf{m}}$	Large gear angular displacement		elastic mesh force coefficient of pinion i
$\omega_{\mathbf{m}}$	large gear angular speed	$\mathbf{K}_{\mathrm{f},\mathrm{i}}, \mathbf{C}_{\mathrm{f},\mathrm{i}}$	elastic mesh torque coefficient of pinion i
$\mathbf{J}_{\mathbf{c},\mathbf{i}}$	i-th pinion inertia after equivlalent coupling-i	$\mathbf{K}_{t,i}, \mathbf{C}_{t,i}$	erastic mesh torque coefficient of pinton-i
$\mathbf{b_{c,i}}$	i-th pinion viscous damped after equivalent	$I_{m,i}$	gear transmission ratio
	coupling-i	$T_1$	The resistant torque of soil and rocks
$\mathbf{J}_{\mathbf{w},\mathbf{i}}$	Inertia of the i-th coupling between reduce-i	$T_2$	The friction torque of soil and rocks which
	and pinion-i	т	The friction torque of soil and rocks which
$\mathbf{b}_{\mathbf{w},\mathbf{i}}$	Viscous damped of the i-th coupling between	13	chafe with the back of the cutterband
	reducer-i and pinion-i	Т	The friction torque of soil and rocks which
$\mathbf{J}_{\mathbf{p},\mathbf{i}}$	i-th pinion inertia;	▲4	chafe with bulkhead
$\mathbf{b}_{\mathbf{p},\mathbf{i}}$	i-th pinion viscous damped	$T_5$	The stirring torque of soil and rocks by cutter-
$\mathbf{T_{e,i}}$	i-th induction motor electrical magnetic torque	0	head stirring rod
$\omega_{\mathbf{p},\mathbf{i}}$	Angular speed of pinion-i	$T_6$	The friction torque of cutterhead bearings and
$\omega_{\mathbf{i}}$	angular speed of induction motor-i	-	sealed chamber

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